

## Fixed Displacement Pumps (ISO System of Units):

$$Q_{pt} = \frac{D_p \times n_p}{1000}$$

$$E_{vp} = \left[ 1 - \frac{P_p}{p_{evpd}} \frac{n_{evpd}}{n_p} (1 - E_{vpd}) \right] \times 100$$

$$Q_{pa} = Q_{pt} \times E_{vp} / 100$$

$$Q_{pL} = Q_{pt} - Q_{pa}$$

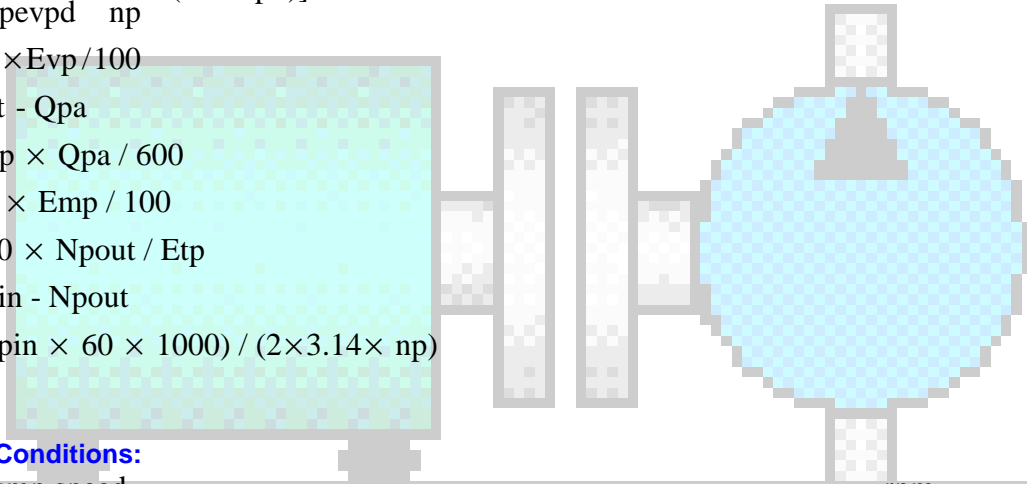
$$N_{pout} = P_p \times Q_{pa} / 600$$

$$E_{tp} = E_{vp} \times E_{mp} / 100$$

$$N_{pin} = 100 \times N_{pout} / E_{tp}$$

$$N_{pL} = N_{pin} - N_{pout}$$

$$T_{shp} = (N_{pin} \times 60 \times 1000) / (2 \times 3.14 \times n_p)$$



### Operating Conditions:

$n_p$	Pump speed	rpm
$P_p$	Pump pressure	bar

### Design Parameter:

$D_p$	Pump displacement	cc/rev
$E_{mp}$	Pump hydro-mechanical efficiency at the operating conditions	%
$E_{vpd}$	Pump volumetric efficiency at specified operating conditions	%
$n_{evpd}$	Pump speed at which efv is defined	rpm
$p_{evpd}$	Pump pressure at which efv is defined	bar

### Output Data:

$E_{vp}$	Pump volumetric efficiency at new operating conditions	%
$Q_{pt}$	Pump theoretical flow rate	L/min
$Q_{pa}$	Pump actual flow rate	L/min
$Q_{pL}$	Pump leakage flow rate	L/min
$E_{tp}$	Pump total efficiency	%
$N_{pout}$	Pump output power	kW
$N_{pL}$	Pump power losses	kW
$N_{pin}$	Pump drive motor power	kW
$T_{shp}$	Torque on the pump shaft	N.m

## Fixed Displacement Motors (ISO System of Units):

$$Q_{mt} = \frac{D_m \times n_m}{1000}$$

$$Q_{ma} = Q_{pt} \times 100 / E_{vm}$$

$$Q_{mL} = Q_{ma} - Q_{pt}$$

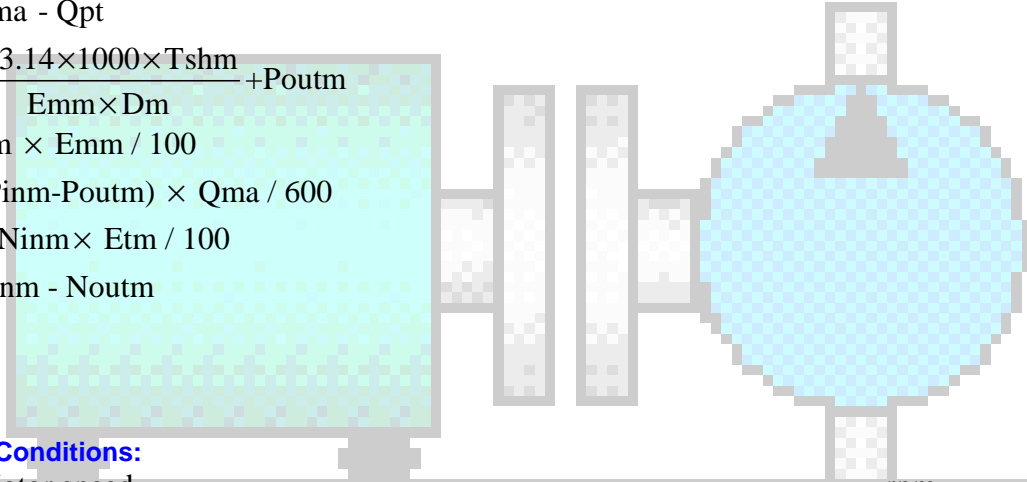
$$P_{inm} = \frac{2 \times 3.14 \times 1000 \times T_{shm}}{E_{mm} \times D_m} + P_{outm}$$

$$E_{tm} = E_{vm} \times E_{mm} / 100$$

$$N_{inm} = (P_{inm} - P_{outm}) \times Q_{ma} / 600$$

$$N_{outm} = N_{inm} \times E_{tm} / 100$$

$$N_{mL} = N_{inm} - N_{outm}$$



### Operating Conditions:

$n_m$	Motor speed	rpm
$P_{outm}$	Motor outlet pressure	bar
$T_{shm}$	Torque on the motor shaft	N.m

### Design Parameter:

$D_m$	Motor displacement	cc/rev
$E_{mm}$	Motor hydro-mechanical efficiency at the operating conditions	%
$E_{vm}$	Motor volumetric efficiency at the operating conditions	%

### Output Data:

$Q_{mt}$	Motor theoretical flow rate	L/min
$Q_{ma}$	Motor actual flow rate	L/min
$Q_{mL}$	Motor leakage flow rate	L/min
$P_{inm}$	Motor inlet pressure	bar
$E_{tm}$	Total motor efficiency	%
$N_{outm}$	Motor output power	kW
$N_{mL}$	Motor power losses	kW
$N_{inm}$	Motor input power	kW

## Double-Acting Hydraulic Cylinder, Static Solution (ISO System of Units):

$$A_{cap} = \pi \times D_{cap}^2 / 4$$

$$AreaRatio = \frac{A_{cap}}{A_{rod}} = \frac{D_{cap}^2}{D_{cap}^2 - D_{rod}^2} \Rightarrow D_{rod} = D_{cap} \sqrt{\frac{AreaRatio - 1}{AreaRatio}}$$

### Extension Stroke Solution: (resistive force applied):

$$P_{cap} = \frac{Prod \times A_{rod}}{A_{cap}} + \frac{9.81 \times F_{cyl}}{10 \times A_{cap}} + \frac{k_{vf} \times V_{cyl}}{10 \times A_{cap}} = \frac{Prod}{AreaRatio} + \frac{9.81 \times F_{cyl}}{10 \times A_{cap}} + \frac{k_{vf} \times V_{cyl}}{10 \times A_{cap}}$$

$$V_{cyl} = [Q_{cap} \times 1000] / [A_{cap} \times 60]$$

$$Stime = Scyl / [V_{cyl} \times 10]$$

$$Q_{rod} = Q_{cap} / AreaRatio$$

### Retraction Stroke Solution: (resistive force applied):

$$Prod = [(10 \times P_{cap} \times A_{cap}) + (9.81 \times F_{cyl}) + (k_{vf} \times V_{cyl})] / [10 \times A_{rod}]$$

$$V_{cyl} = [Q_{rod} \times 1000] / [A_{rod} \times 60]$$

$$Stime = Scyl / [V_{cyl} \times 10]$$

$$Q_{cap} = Q_{rod} \times AreaRatio$$

### Cylinder Dimensions:

Dcap	Cylinder bore	mm
Drod	Rod diameter	mm
Acap	Effective area at the cap side	cm <sup>2</sup>
Arod	Effective area at the rod side	cm <sup>2</sup>
Scyl	Cylinder stroke	mm

### Cylinder Hydraulics:

Pcap	Working pressure at the cap side	bar
Prod	Working pressure at the rod side	bar
Qcap	Flow rate at cap side	L/min
Qrod	Flow rate at rod side	Lmin

### Cylinder Dynamics:

Fcyl	Equivalent resistive force acts on the cylinder rod	kgf
Vcyl	Cylinder speed	cm/s
k <sub>vf</sub>	Viscous friction coefficient	N/(cm/s)
Stime	Time required to reach end of the cylinder stroke	s

## Hydraulic Cylinder Buckling Calculations, (ISO System of Units):

$$J_{rod} = \frac{\pi \times D_{rod}^4}{64 \times 1000^4}$$

$$S_{Ratio} = 4 \times \text{Elength} / D_{rod}$$

$$C_{SRatio} = \pi \sqrt{\frac{E_{rod}}{0.8 \times Y_{Mrod}}}$$

Euler's Equation (long cylinder strokes - elastic deformation period)

if  $S_{Ratio} > C_{SRatio}$ :

$$B_{load} = \frac{\pi^2 \times E_{rod} \times 10^6 \times J_{rod} \times 100^2}{\text{Elength}^2 \times 9.81 \times 1000}$$

$$A_{load} = B_{load} / SF$$

### Input Data:

Drod	Rod diameter	mm
Erod	Modulus of elasticity of cylinder rod	MPa
YMrod	Yield Strength of cylinder rod	MPa
SF	Safety Factor	-
Alength	Actual compressed length	cm
-	Load attachment to the cylinder rod	-

### Output Data:

Elength	Effective length	cm
Jrod	Second moment of area	m <sup>4</sup>
Bload	Critical buckling load	Ton
Aload	Allowable compressive load	Ton
SRatio	Slenderness Ratio	-
CSRatio	Critical slenderness ratio	-

### Assumptions:

Load acting axially and cylinder rod is not subjected to side loads

## Hydraulic Smooth Lines (Pipes/Tubes/Hoses) (ISO System of Units):

$$A_{line} = (\pi \times D_{line}^2) / (4 \times 100)$$

$$V_{line} = (1000 \times Q_{line}) / (A_{line} \times 60 \times 100)$$

$$Re = \frac{1000 \times V_{line} \times D_{line}}{\text{Viscosity}}$$

$$\text{Flow is Laminar} \rightarrow F_{Cline} = 64 / Re$$

$$\text{Flow is Turbulent} \rightarrow F_{Cline} = 0.316 / Re^{0.25}$$

$$D_{Pline} = F_{Cline} \times \frac{\text{Density}}{2} \times \frac{L_{line} \times 1000}{D_{line}} \times \frac{V_{line}^2}{10^5}$$

### Operating Conditions:

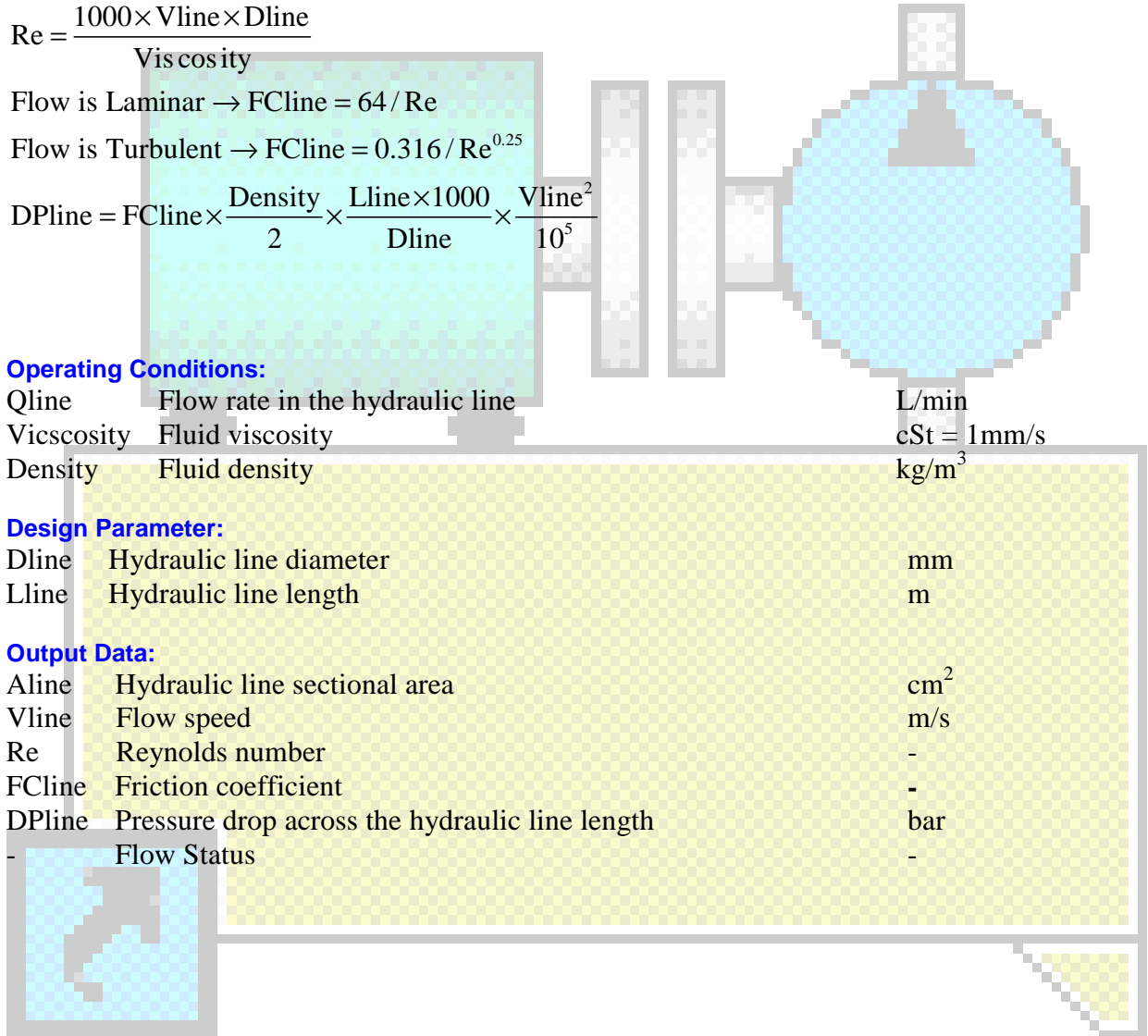
Qline	Flow rate in the hydraulic line	L/min
Viscosity	Fluid viscosity	cSt = 1mm/s
Density	Fluid density	kg/m <sup>3</sup>

### Design Parameter:

Dline	Hydraulic line diameter	mm
Lline	Hydraulic line length	m

### Output Data:

Aline	Hydraulic line sectional area	cm <sup>2</sup>
Vline	Flow speed	m/s
Re	Reynolds number	-
FCline	Friction coefficient	-
Dpline	Pressure drop across the hydraulic line length	bar
-	Flow Status	-



## Accumulator (ISO System of Units):

Piston Accumulator →  $P_0 = P_1 - 5$

Bladder/Diaphragm accumulator →  $P_0 = 0.85 \times P_1$

If gas thermal process is isothermal then

$$V_1 = V_0 \left[ \frac{P_0}{P_1} \right] \quad \text{and} \quad V_2 = V_0 \left[ \frac{P_0}{P_2} \right]$$

If gas thermal process is adiabatic then

$$V_1 = V_0 \left[ \frac{P_0}{P_1} \right]^{\frac{1}{AE}} \quad \text{and} \quad V_2 = V_0 \left[ \frac{P_0}{P_2} \right]^{\frac{1}{AE}}$$

$$DV = V_2 - V_1$$

$$ACHT = \frac{DV \times 60}{Q_{\text{pump}}} \quad ACHP = \frac{Q_{\text{pump}} \times \frac{P_1 + P_2}{2}}{600}$$

### Operating Conditions:

P1	Minimum system absolute pressure	bar
P2	Maximum system absolute pressure	bar
AE	Adiabatic exponent	

### Design Parameter:

V0	Accumulator nominal volume	Liter
Qpump	Pump flow rate	L/min

### Output Data:

P0	Accumulator pre-charge absolute pressure	bar
V1	Gas volume at P1	Liter
V2	Gas volume at P2	Liter
DV	Oil stored volume	Liter
ACHT	Accumulator charging time	s
ACHP	Accumulator charging power	kW

### Note:

For bladder/diaphragm, maximum pressure ratio  $P_2/P_0$  should be respected

## Conversion Factors:

### Distance:

1 mm =	0.03937008	in
1 cm =	0.3937008	in
1 m =	3.28084	ft

### Area:

1 cm <sup>2</sup> =	0.1550003	in <sup>2</sup>
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### Volume:

1 Liter =	61.02374	in <sup>3</sup>
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### Speed:

1 cm/s =	0.3937008	in/s
1 m/s =	3.28084	f/s

### Force:

1 kgf =	2.204623	lbf
1 Ton =	2204.623	lbf

### Work/Energy/Torque

1 N.m =	0.73756	lb.ft
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### Power:

1 kW =	1.36	HP
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### Pressure / Modulus of Elasticity

1 bar =	14.6	psi
1 MPa =	145.0377	psi

### Pump/Motor Displacement:

1 cc/rev =	0.06102374	in <sup>3</sup> /rev
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### Flow Rate:

1 L/min =	0.2641721	gpm
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### Density:

1 kg/m <sup>3</sup> =	0.06242796	lb/ft <sup>3</sup>
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### Viscous Friction:

1 N/(cm/s) =	0.571	lbf/(in/s)
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